CIRF Circuit Intégré Radio Fréquence

Lecture I

Introduction
Baseband Pulse Transmission
Digital Passband Transmission
Circuit Non-idealities Effect

Hassan Aboushady Université Paris VI

CIRF Circuit Intégré Radio Fréquence

Lecture I

Introduction
Baseband Pulse Transmission
Digital Passband Transmission
Circuit Non-idealities Effect

Hassan Aboushady Université Paris VI

Wireless Systems

Direct conversion architecture



- Transmitter issues
 - Meeting the spectral mask (LO phase noise & feedthrough, quadrature accuracy), D/A accuracy, power amp linearity
- Receiver Issues
 - Meeting SNR (Noise figure, blocking performance, channel selectivity, LO phase noise, A/D nonlinearity and noise), selectivity (filtering), and emission requirements

Future Goals

- Low cost, low power, and small area solutions
 - New architectures and circuits!
- Increased spectral efficiency
 - Example: GSM cellphones (GMSK) to 8-PSK (Edge)
 - Requires a linear power amplifier!
- Increased data rates
 - Example: 802.11b (11 Mb/s) to 802.11a (> 50 Mb/s)
 - GFSK modulation changes to OFDM modulation
- Higher carrier frequencies
 - 802.11b (2.5 GHz) to 802.11a (5 GHz) to ? (60 GHz)
- New modulation formats
 - GMSK, CDMA, OFDM, pulse position modulation
- New application areas

High Speed Data Links

A common architecture



- Transmitter Issues
 - Intersymbol interference (limited bandwidth of IC amplifiers, packaging), clock jitter, power, area
- Receiver Issue
 - Intersymbol interference (same as above), jitter from clock and data recovery, power, area

Future Goals

- Low cost, low power, small area solutions
 - New architectures and circuits!
- Increased data rates
 - 40 Gb/s for optical (moving to 120 Gb/s!)
 - Electronics is a limitation (optical issues getting significant)
 - > 5 Gb/s for backplane applications
 - The channel (i.e., the PC board trace) is the limitation
- High frequency compensation/equalization
 - Higher data rates, lower bit error rates (BER), improved robustness in the face of varying conditions
 - How do you do this at GHz speeds?
- Multi-level modulation
 - Better spectral efficiency (more bits in given bandwidth)

What are the Issues with Wireless Systems?

- Noise
 - Need to extract the radio signal with sufficient SNR
- Selectivity (filtering, processing gain)
 - Need to remove interferers (which are often much larger!)
- Nonlinearity
 - Degrades transmit spectral mask
 - Degrades selectivity for receiver

Multidisciplinarity of radio design





- S. Haykin, "Communication Systems", Wiley 1994.
- B. Razavi, "RF Microelectronics", Prentice Hall, 1997.
- M. Perrott, "High Speed Communication Circuits and Systems", M.I.T.OpenCourseWare, http://ocw.mit.edu/, Massachusetts Institute of Technology, 2003.
- D. Yee, "A Design methodology for highly-integrated low-power receivers for wireless communications", http://bwrc.eecs.berkeley.edu/, Ph.D. University of California at berkeley, 2001.

CIRF Circuit Intégré Radio Fréquence

Lecture I

Introduction
Baseband Pulse Transmission
Digital Passband Transmission
Circuit Non-idealities Effect

Hassan Aboushady University of Paris VI

Digital Baseband Transmission

Major sources of errors in the detection of transmitted digital data:

ISI : InterSymbol Interference

The result of data transmission over a non-ideal channel is that each received pulse is affected by adjacent pulses.



- Vout

Channel Noise

Detecting a pulse transmitted over a channel that is corrupted by additive noise.



Matched Filter



g(t): transmitted pulse signal, binary symbol `1' or `0'.
w(t): channel noise, sample function of a white noise process of zero mean and power spectral density N₀/2.

$$x(t) = g(t) + w(t) \quad , \quad 0 \le t \le T \qquad \qquad h(t) \qquad \qquad y(t) = g_0(t) + n(t)$$

- Filter Requirements, *h*(*t*) :
 - Make the instantaneous power in the output signal $g_{\theta}(t)$, measured at time t=T, as large as possible compared with the average power of the output noise, n(t).

H. Aboushady

Maximize Signal-to-Noise Ratio



Objective :

Specify the impulse response h(t) of the filter such that the output signal-to-noise ratio is maximized.

H. Aboushady

Math Review

Fourier Transform

$$G(f) = \int_{-\infty}^{\infty} g(t) \quad e^{-j 2\pi f t} dt$$

Inverse Fourier Transform

$$g(t) = \int_{-\infty}^{\infty} G(f) \quad e^{j 2\pi f t} df$$

Power Spectral Density of a Random Process *S_X(f)* **applied to a Linear System** *H(f)*

$$S_{Y}(f) = \left| H(f) \right|^{2} S_{X}(f)$$

H. Aboushady

Compute Signal-to-Noise Ratio

Signal Power

$$g_0(t) = \int_{-\infty}^{\infty} H(f) G(f) e^{j 2\pi f t} df$$

$$\left| \left| g_0(T) \right|^2 = \left| \int_{-\infty}^{\infty} H(f) G(f) e^{j 2\pi f T} df \right|^2$$

Noise Power

$$S_N(f) = \frac{N_0}{2} \left| H(f) \right|^2$$

$$\overline{n^2(t)} = \int_{-\infty}^{\infty} S_N(f) \, df$$

$$\overline{n^2(t)} = \frac{N_0}{2} \int_{-\infty}^{\infty} \left| H(f) \right|^2 df$$

Signal-to-Noise Ratio

Optimization Problem: For a given G(f), find H(f)in order to maximize SNR.

$$SNR = \frac{\left| \int_{-\infty}^{\infty} H(f) G(f) e^{j 2\pi f T} df \right|^{2}}{\frac{N_{0}}{2} \int_{-\infty}^{\infty} \left| H(f) \right|^{2} df}$$

H. Aboushady

Schwarz's Inequality

• If we have 2 complex functions $\phi_1(x)$ and $\phi_2(x)$ in the real variable x, satisfying the conditions:

$$\int_{-\infty}^{\infty} \left| \phi_1(x) \right|^2 \, dx < \infty$$

$$\int_{-\infty}^{\infty} \left| \phi_2(x) \right|^2 \, dx < \infty$$

then we may write that:

$$\left\| \int_{-\infty}^{\infty} \phi_1(x) \phi_2(x) dx \right\|^2 \leq \int_{-\infty}^{\infty} |\phi_1(x)|^2 dx \int_{-\infty}^{\infty} |\phi_2(x)|^2 dx \quad \text{iff} \quad \phi_1(x) = k \phi_2^*(x) \text{ where } k : \text{arbitrary constant}$$
setting:
$$\phi_1(x) = H(f) \quad \text{and} \quad \phi_2(x) = G(f) e^{j2\pi fT}$$

$$\left\| \int_{-\infty}^{\infty} H(f) G(f) e^{j2\pi fT} df \right\|^2 \leq \int_{-\infty}^{\infty} |H(f)|^2 df \int_{-\infty}^{\infty} |G(f)|^2 df$$

H. Aboushady

 $|\mathbf{J}|_{-\infty}$

Matched Filter

$$SNR \leq \frac{2}{N_0} \int_{-\infty}^{\infty} |G(f)|^2 df$$

$$\phi_1(x) = k \phi_2^*(x)$$

$$H_{opt}(f) = k G^*(f) e^{-j2\pi f(T-t)} df$$

$$h_{opt}(t) = k \int_{-\infty}^{\infty} G^*(f) e^{-j2\pi f(T-t)} df$$

 for a real signal g(t) we have G*(f)=G(-f)

$$h_{opt}(t) = k g(T - t)$$

• The impulse response of the optimum filter, except for the scaling factor k, is a time-reversed and delayed version of the input signal g(t)

H. Aboushady

Properties of Matched Filters

$$h_{opt}(t) = k g(T - t)$$
$$H_{opt}(f) = k G^{*}(f) e^{-j 2\pi f T}$$

$$G_{0}(f) = H_{opt}(f) G(f)$$

= $k G^{*}(f) G(f) e^{-j 2\pi f T}$
= $k |G(f)|^{2} e^{-j 2\pi f T}$

• Taking the inverse Fourier transform at *t*=*T*:

$$g_0(T) = \int_{-\infty}^{\infty} G_0(f) e^{j2\pi fT} df = k \int_{-\infty}^{\infty} |G(f)|^2 df = k E$$
 Where E is the energy of the pulse signal $g(t)$

$$\overline{n^{2}(t)} = \frac{N_{0}}{2} \int_{-\infty}^{\infty} \left| H(f) \right|^{2} df \qquad \qquad \overline{n^{2}(t)} = \frac{N_{0}}{2} k^{2} \int_{-\infty}^{\infty} \left| G(f) \right|^{2} df = k^{2} \frac{N_{0}}{2} E$$

$$SNR_{\text{max}} = \frac{k^2 E^2}{k^2 \frac{N_0}{2} E} = \frac{2 E}{N_0}$$

H. Aboushady

Matched Filter for Rectangular Pulse



H. Aboushady

Error Rate due to Noise



T_b is the bit duration, A is the transmitted pulse amplitude

- The receiver has prior knowledge of the pulse shape but not its polarity.
- There are two possible kinds of error to be considered:
 (1) Symbol `1' is chosen when a `0' was transmitted.
 (2) Symbol `0' is chosen when a `1' was transmitted.

Suppose that symbol `0' was sent: x(t) = -A + w(t), $0 \le t \le T_b$

The matched filter output is:
$$Y = \frac{1}{T_b} \int_0^{T_b} x(t) dt = -A + \frac{1}{T_b} \int_0^{T_b} w(t) dt$$

Y is a random variable with Gaussian distribution and a mean of *-A*.

The variance of Y:
$$\sigma_Y^2 = \overline{(Y+A)^2} = \frac{1}{T_b^2} \int_0^{T_b} \int_0^{T_b} R_W(t,u) dt du$$

Where $R_W(t,u)$ is the autocorrelation function of the white noise w(t). Since w(t) is white with a PSD of $N_0/2$:

$$R_{W}(t,u) = \frac{N_{0}}{2} \delta(t-u)$$

$$\sigma_{Y}^{2} = \frac{N_{0}}{2 T_{b}}$$

H. Aboushady

PDF: Probability Density Function





• Symbol '0' was sent: $\mu_Y = -A$, $\sigma_Y^2 = \frac{N_0}{2T_b}$ $f_Y(y \mid \mathbf{0})$ $P_{e0} = P(y > \lambda | \text{symbol '0' was sent})$ P.0 $= \int f_{Y}(y|0) \, dy$ -A(a)• Symbol `1' was sent: $\mu_Y = +A$, $\sigma_Y^2 = \frac{N_0}{2T_h}$ $f_{Y}(y|1)$ $P_{e0} = P(y < \lambda | \text{symbol '1' was sent})$ Pet $= \int f_{Y}(y|1) \, dy$ A

H. Aboushady

(bUniversity of Paris VI

٦Ľ

BER in a PCM receiver

$$P_{e0} = \frac{1}{\sqrt{\pi N_0 / T_b}} \int_{\lambda}^{\infty} \exp\left[-\frac{(y+A)^2}{N_0 / T_b}\right] dy$$

• let $\lambda = \theta$ and the probabilities of binary symbols: $p_{\theta} = p_1 = 1/2$.

$$z = \frac{y + A}{\sqrt{N_0 / T_b}} \qquad \qquad P_{e0} = \frac{1}{\sqrt{\pi}} \int_{\sqrt{E_b / N_0}}^{\infty} \exp\left[-z^2\right] dz$$

• where $E_b = A^2 T_b$, is the transmitted signal energy per bit.

• the complementary error function:

$$erfc(u) = \frac{1}{\sqrt{\pi}} \int_{u}^{\infty} \exp\left[-z^{2}\right] dz$$

$$P_{e1} = P_{e0} = \frac{1}{2} \operatorname{erfc}\left(\sqrt{\frac{E_b}{N_0}}\right)$$

$$P_{e} = p_{0}P_{e0} + p_{1}P_{e1}$$

$$P_{e0} = P_{e1}$$

$$p_{0} = p_{1} = \frac{1}{2}$$

$$P_{e} = P_{e0} = P_{e1}$$





University of Paris VI

CIRF Circuit Intégré Radio Fréquence

Lecture I

Introduction
Baseband Pulse Transmission
Digital Bandpass Transmission
Circuit Non-idealities Effect

Hassan Aboushady Université Paris VI

Why Modulation?

- In wired systems, coaxial lines exhibit superior shielding at higher frequencies
- In wireless systems, the antenna size should be a significant fraction of the wavelength to achieve a reasonable gain.
- Communication must occur in a certain part of the spectrum because of FCC regulations.
- Modulation allows simpler detection at the receive end in the presence of non-idealities in the communication channel.

Message Source



- m_i : one symbol every *T* seconds
- Symbols belong to an alphabet of *M* symbols: *m*₁, *m*₂, ..., *m*_M
- Message output probability:

$$P(m_1) = P(m_2) = \dots = P(m_M)$$
$$p_i = P(m_i) = \frac{1}{M}$$

• Example: Quaternary PCM, 4 symbols: 00, 01, 10, 11

H. Aboushady

Transmitter



• Signal Transmission Encoder: produces a vector s_i made up of N real elements, where $N \le M$.

• <u>Modulator</u>: constructs a distinct signal $s_i(t)$ representing m_i of duration T.

• Energy of
$$s_i(t)$$
: $E_i = \int_0^T s_i^2(t) dt, \quad i = 1, 2, ..., M$

• *s_i(t)* is real valued and transmitted every T seconds.

Examples of Transmitted signals: $s_i(t)$

• The modulator performs a step change in the amplitude, phase or frequency of the sinusoidal carrier



Communication Channel



- Two Assumptions:
 - •The channel is linear (no distortion).
 - *s_i(t)* is perturbed by an Additive, zero-mean, stationnary, White, Gaussian Noise process (AWGN).
- **Received signal** *x*(*t*) :

$$x(t) = s_i(t) + w(t), \quad \begin{cases} 0 \le t \le T \\ i = 1, 2, ..., M \end{cases}$$



H. Aboushady

Receiver



•TASK: observe received signal, x(t), for a duration T and make a best estimate of transmitted symbol, m_i .

•<u>Detector</u>: produces observation vector x .

•<u>Signal Transmission Decoder</u>: estimates \hat{m} using x, the modulation format and $P(m_i)$.

• The requirement is to design a receiver so as to minimize the average probability of symbol error:

$$P_e = \sum_{i=1}^{M} P(\hat{m} \neq m_i) P(m_i)$$

H. Aboushady

Coherent and Non-Coherent Detection



- Coherent Detection:
 - The receiver is time synchronized with the transmitter.
 - The receiver knows the instants of time when the modulator changes state.
 - The receiver is phase-locked to the transmitter.
- Non-Coherent Detection:
 - No phase synchronism between transmitter and receiver.

Gram-Schmidt Orthogonalization Procedure

• we represent the given set of realvalued energy signals $s_1(t), s_2(t), \dots, s_M(t)$, each of duration T:

$$s_i(t) = \sum_{j=1}^N s_{ij} \phi_j(t) \quad , \quad \begin{cases} 0 \le t \le T \\ i = 1, 2, \dots, M \end{cases}$$

• where the coefficients of the expansion are defined by:

$$s_{ij} = \int_{0}^{T} s_{i}(t) \phi_{j}(t) dt \quad , \quad \begin{cases} i = 1, 2, \dots, M \\ j = 1, 2, \dots, N \end{cases}$$

• the real-valued basis functions $\phi_1(t)$, $\phi_2(t)$, ..., $\phi_N(t)$ are orthonormal:

$$\int_{0}^{T} \phi_{i}(t) \phi_{j}(t) dt = \begin{cases} 1 & if \quad i = j \\ 0 & if \quad i \neq j \end{cases}$$

H. Aboushady



Coherent Detection of Signals in Noise



where *w* is the noise vector.

H. Aboushady

Coherent Binary PSK:

•
$$M=2, N=1$$

 $0 \le t \le T_b$ $s_1(t) = \sqrt{\frac{2E_b}{T_b}} \cos(2\pi f_c t)$ $s_2(t) = \sqrt{\frac{2E_b}{T_b}} \cos(2\pi f_c t + \pi)$

• To ensure that each transmitted bit contains an integral number of cycles of the carrier wave, fc =nc/Tb, for some fixed integer nc.

• One basis function: $\phi_1(t) = \sqrt{\frac{2}{T_b}} \cos(2\pi f_c t)$, $0 \le t \le T_b$

• Signal constellation consists of two message points:

$$s_{11} = \int_{0}^{T_{b}} s_{1}(t) \phi_{1}(t) dt = \sqrt{E_{b}}$$
$$s_{21} = \int_{0}^{T_{b}} s_{2}(t) \phi_{1}(t) dt = -\sqrt{E_{b}}$$



H. Aboushady

Generation and Detection of Coherent Binary PSK





Coherent QPSK:

• *M*=4, *N*=2:

$$s_{i}(t) = \begin{cases} \sqrt{\frac{2E}{T}} \cos\left[2\pi f_{c}t + (2i-1)\frac{\pi}{4}\right] , & 0 \le t \le T \\ 0 & , \text{ elsewhere} \end{cases}$$

$$s_{1}(t) = \sqrt{\frac{2E}{T}} \cos(2\pi f_{c}t + \frac{\pi}{4})$$

$$s_{2}(t) = \sqrt{\frac{2E}{T}} \cos(2\pi f_{c}t + 3\frac{\pi}{4})$$

$$s_{3}(t) = \sqrt{\frac{2E}{T}} \cos(2\pi f_{c}t + 5\frac{\pi}{4})$$

$$s_{4}(t) = \sqrt{\frac{2E}{T}} \cos(2\pi f_{c}t + 7\frac{\pi}{4})$$

• Two basis function:
$$\phi_1(t) = \sqrt{\frac{2}{T}} \cos(2\pi f_c t)$$
, $0 \le t \le T$
 $\phi_2(t) = \sqrt{\frac{2}{T}} \sin(2\pi f_c t)$, $0 \le t \le T$
Aboushady

Н.

rsity of Paris VI

Constellation Diagram of Coherent QPSK System



H. Aboushady

QPSK waveform: 01101000



H. Aboushady

Generation and Detection of Coherent QPSK Signals



Power Spectra of BPSK , QPSK and M-ary PSK

• Symbol Duration:

$$T = T_b \log_2 M$$

• Power Spectral Density of an M-ary PSK signal:

$$S_B(f) = 2E \operatorname{sinc}^2(Tf)$$
$$= 2E_b \log_2 M \operatorname{sinc}^2(T_b f \log_2 M)$$



CIRF Circuit Intégré Radio Fréquence

Lecture I

Introduction
Baseband Pulse Transmission
Digital Passband Transmission
Circuit Non-idealities Effect

Hassan Aboushady Université Paris VI

QPSK Receiver



H. Aboushady

Receiver Circuit Non-Idealities

Circuit Noise (Thermal, 1/f) Gain Mismatch Phase Mismatch DC Offset Frequency Offset Local Oscillator phase noise

Circuit Noise

Circuit Noise:

- Thermal Noise
 - Resistors
 - Transistors
- Flicker (1/f) Noise
 MOS transistors





H. Aboushady

University of Paris VI

Gain Mismatch



H. Aboushady

Phase Mismatch



DC Offset



H. Aboushady





H. Aboushady

Local Oscillator Phase Noise



H. Aboushady

Reciprocal Mixing

